

Historical and Current Rheological Binder Characterization vs. Binder Performance

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Why Characterize Binder Rheology With Mathematical Models?

- ⇒ Provide mathematical formula that can be manipulated for purpose of calculation
- ⇒ Provide quantitative parameters that can be used to characterize rheology and changes in rheology
- ⇒ Provide rational basis for specification criteria
- ⇒ Provide link between binder and mixture

Models – What Is Needed?

- ⇒ Needs vary with application
- ⇒ From binder perspective binder need model that:
 - Captures changes in binder rheology caused by long-term aging
 - Must be compatible with molecular/structure changes at molecular level
- ⇒ Links binder and mixture properties
- ⇒ Is related to binder “quality” – a forgotten issue
- ⇒ Many possibilities – focus on CA model

Explicit Models – Pre SHRP

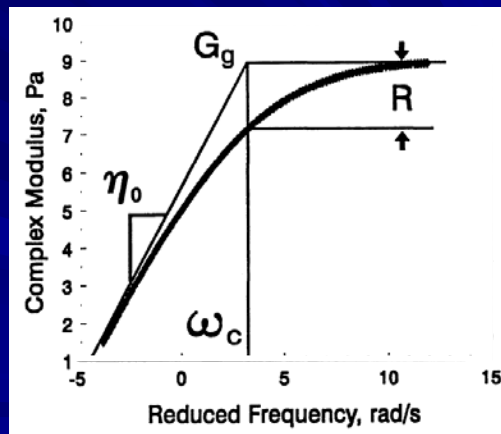
- ⇒ Jongepier and Kuilman
 - Relaxation spectra as log normal distribution
- ⇒ Dobson (1969)
 - Based on empirical relationships between modulus and phase angle
- ⇒ Dickenson and DeWitt (1974)
 - Based on hyperbolic representation
 - Recognized relaxation spectra skewed

Models – Christensen-Anderson

- ⇒ Developed during SHRP
- ⇒ Genesis was the need to describe relaxation modulus
 - All other rheological functions can be generated from relaxation modulus
- ⇒ Christensen recognized that relaxation modulus is skewed, not symmetric
 - Concluded that skewed function was needed

CA Model

- ⇒ Christensen-Anderson - CA model (1993)
 - Relates $G^*(\omega)$ to G_g , ω_c and R



Weibul Function to Model Relaxation Spectrum

$$F(x) = \frac{m}{b} \exp\left\{\frac{x-a}{b}\right\} \left[1 + \left\{\frac{x-a}{b}\right\}\right]^{-(m+1)}$$

$F(x)$ = Probability density function

m = Skewness parameter

x = Independent parameter

b = Scale parameter

a = Location parameter

Cumulative Weibull Function

⇒ Integrate to obtain cumulative function:

$$P(x) = 1 - \left[1 - \left\{\frac{x-a}{b}\right\} b\right]^{-m}$$

⇒ or:

$$1 - P(x) = \left[1 + \left\{\frac{x-a}{b}\right\} b\right]^{-m}$$

CA Model for $G^*(\omega)$

⇒ Substituting rheological parameters:

$$G^*(\omega) = G_g \left[1 + \left\{ \frac{\omega}{\omega_c} \right\}^{(\log 2 / R)} \right]^{-R / \log 2}$$

$G^*(\omega)$ = Measured complex modulus

G_g = Glassy modulus

R = Rheological Index (shape factor)

ω = Test frequency

ω_c = Crossover frequency (location parameter)

CA Model for $\delta(\omega)$

⇒ Rewriting and substituting rheological parameters:

$$\delta(\omega) = 90 / \left[1 + \left\{ \frac{\omega}{\omega_c} \right\}^{(\log 2) / R} \right]$$

$\delta(\omega)$ = Measured phase angle

Temperature Dependency

- ⇒ WLF based on free volume concepts
 - Good results above T_g
- ⇒ Arrhenius based on rate theory
 - Necessary below glass transition temperature
- ⇒ Polynomial
 - Useful over small temperature range only
 - Works well with BBR data

R and Delayed Elastic Response

$$1/G^*(\omega) = 1/G_E + 1/G_{DE}(\omega) + 1/G_V(\omega)$$

$$1/G_{DE}(\omega) = 1/G^*(\omega) - 1/G_E - 1/G_V(\omega)$$

↓
Measured
at some T
and ω

↓
 $1/G_g$

↓
 $1/(\omega\eta_0)$

Estimate for Rheological Index

⇒ Model can be rewritten as:

$$\log G^*(\omega) = \log G_g + (R / \log 2) \log[1 - \delta(\omega) / 90]$$

⇒ $G^*(\omega)$ versus $\log[1 - \delta(\omega) / 90]$

– slope $R/\log 2$

– Can be estimated from a single DSR measurement

⇒ Relationship works well when:

$$10^\circ < \delta(\omega) < 70^\circ$$

Estimation of η_0 and ω_c

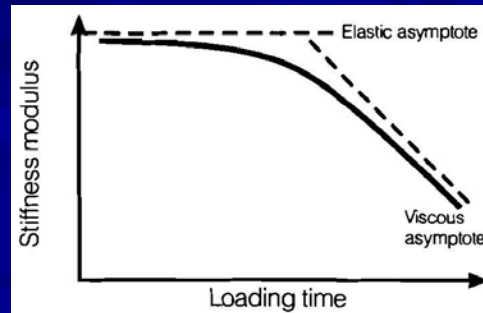
⇒ Similar shortcuts

⇒ Full mastercurve is not needed to estimate model [parameters

⇒ Useful in following aging studies

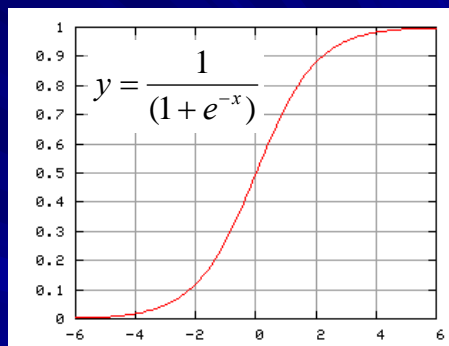
Other Models – van der Poel

- ⇒ Predicts stiffness from Pen and vis
- ⇒ Recognized hyperbolic relationship S vs. T
- ⇒ Model implicit in development of nomograph
 - Viscous asymptote
 - Elastic asymptote



Mix models - Witczak

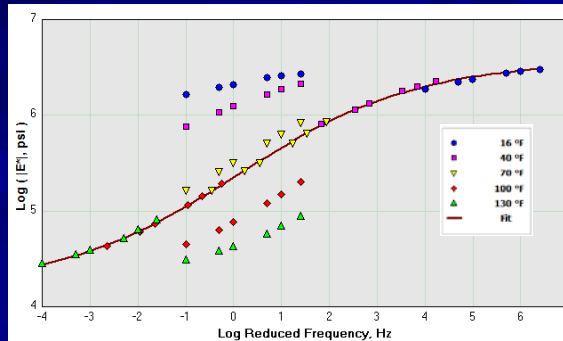
- ⇒ Basic symmetric sigmoid function
- ⇒ Basis of Witczak model for asphalt mixture E^* data



Witczak model

$$\log(E^*) = \delta + \frac{\alpha}{1 + e^{\beta + \gamma(\log t_r)}}$$

- ⇒ Two asymptotes and the central/inflection point of the sigmoid
- ⇒ Model is limited in shape to a symmetrical sigmoid



Temperature Susceptibility Parameters

- ⇒ $PI_{R\&B}$ (Pfeiffer and van Doormaal, 1936)
 - Ring and ball and pen
- ⇒ $PI_{\log Pen}$ (Huekelom and Klomp, 1964)
 - Slope of log pen vs temperature
- ⇒ PVN (McLeod, 1972)
 - Pen at 25°C and viscosity at 60 or 135 60°C
- ⇒ VTS (Puzinauskas)
 - Viscosity at 60 and 135 60°C

Comments - Temperature Susceptibility Parameters

- ⇒ Based on measurements at two temperatures
- ⇒ Shear rates not same at multiple temperatures
- ⇒ Confound time and temperature effects
- ⇒ Studies show that different indices are not equivalent and vary differently with aging
 - Indices reflect time and temperature susceptibility

Temperature Susceptibility

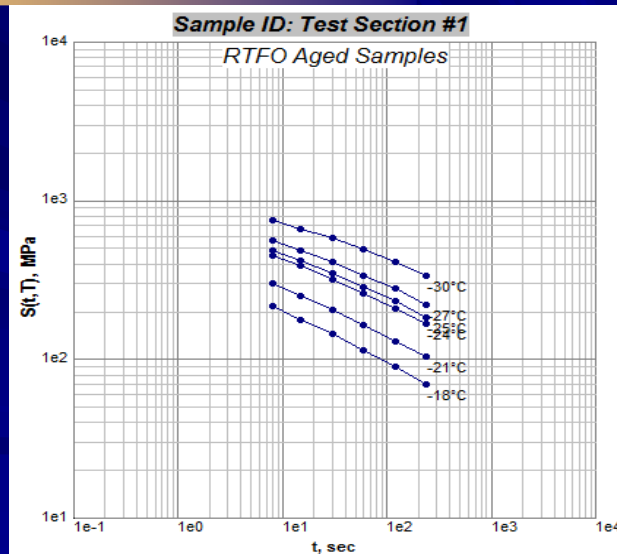
- ⇒ In old specifications captures via PI, PVN etc
- ⇒ How do we capture this in the newer specifications/testing
- ⇒ Example – five data sets from Lamont Road

BBR data using CAM Model

- ⇒ Analysis of 5 data examples from Lamont test road
- ⇒ Master curve construction using AASHTO PP42
 - CAM model

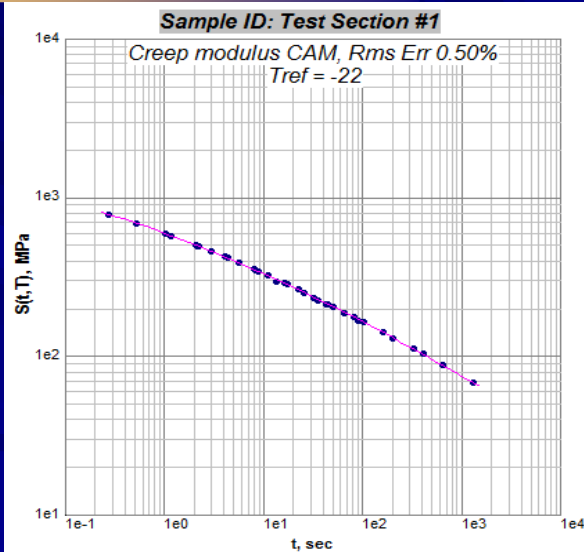
BBR data

- ⇒ Five sections considered
- ⇒ Typical example of data
- ⇒ Used all data available



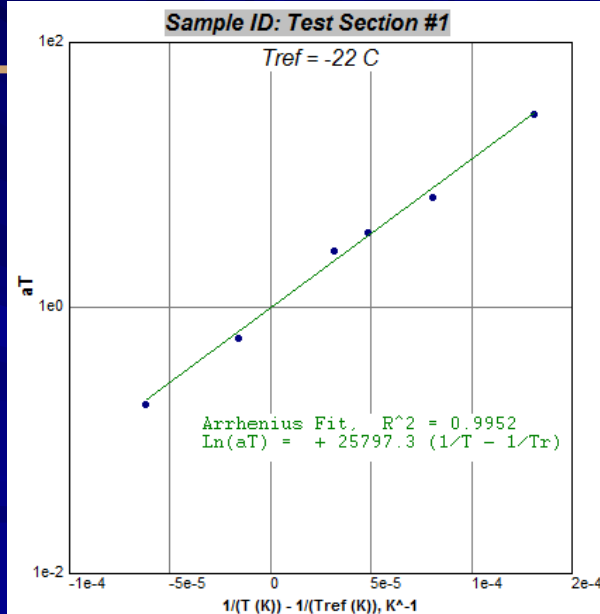
Master Curve Construction

⇒ Used AASHTO PP42 to construct master curves



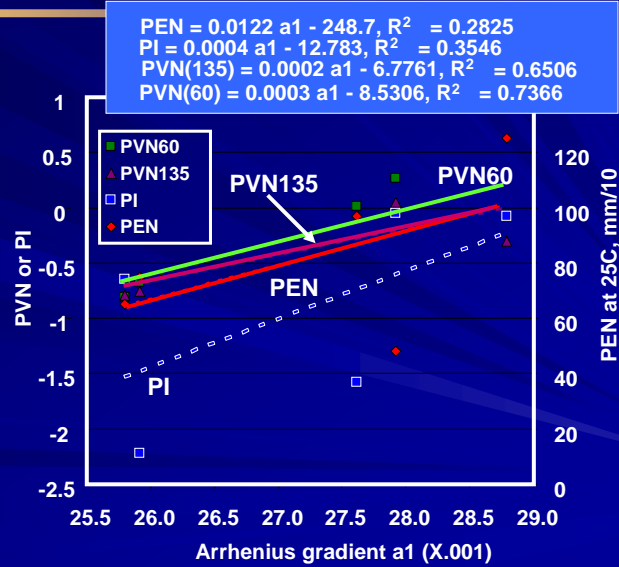
Shift factors

⇒ Shift factors obtained in Arrhenius form



Temperature susceptibility

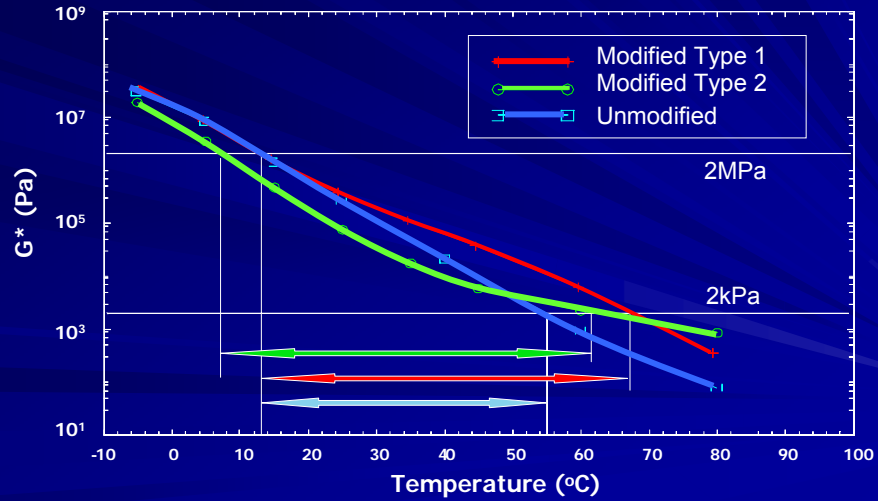
- ⇒ The temperature susceptibility is captured in the slope of the shift factor
- ⇒ The better r^2 results from the data obtained to compute the empirical parameter closest to the rheological measurements



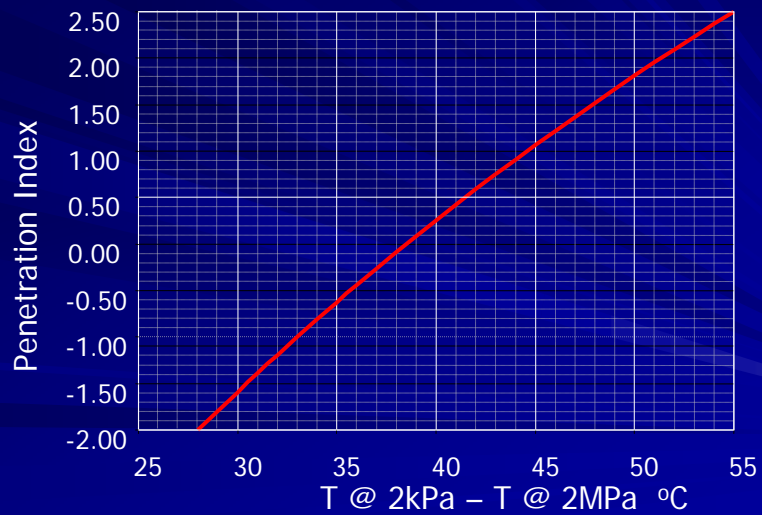
Temperature intervals

- ⇒ Similar to US absolute grade (PG)
- ⇒ Used in Europe – particularly UK

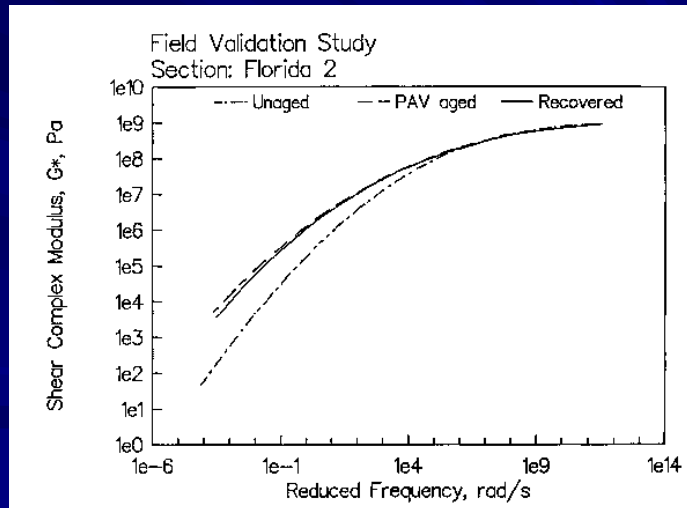
PI can be related to temp interval



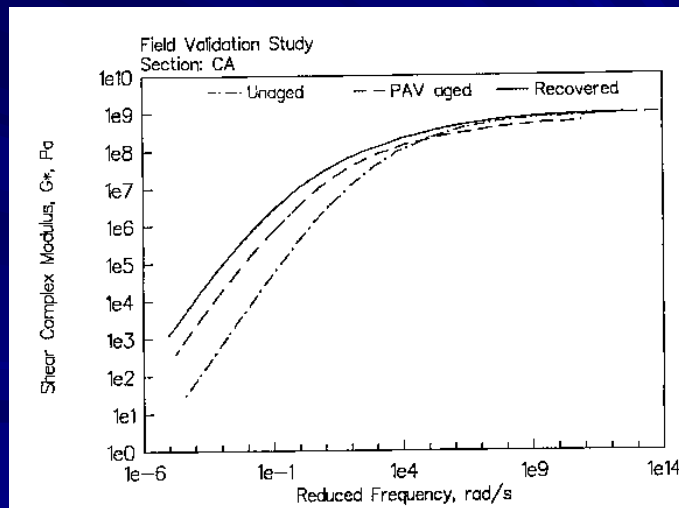
Penetration Index from DSR Data



Model Parameter Changes with Aging



Model Parameter Changes with Aging



R and ω_c May Both Change

- ⇒ Changes in R reflect changes in relaxation Modulus
 - Shape of mastercurve
- ⇒ Changes in Infinite number of combinations ω_c reflect hardening
 - Location of mastercurve

Closing Comments

- ⇒ Many different models are available for characterizing rheological properties of binders
 - Model selected depends on application
- ⇒ Skewed function is needed to model mastercurve
- ⇒ Shortcut methods can be used to generate CA model parameters
- ⇒ Temperature Susceptibility parameters can be related to CA model parameters
- ⇒ R and or ω_c can change with aging

Acknowledgements

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